

**FAILURE MODES EFFECTS ANALYSIS (FMEA) -- CIL HARDWARE****NUMBER:03-1-0257 -X****SUBSYSTEM NAME:** MAIN PROPULSION**REVISION:** 4 11/08/00**PART DATA**

	<b>PART NAME</b>	<b>PART NUMBER</b>
	<b>VENDOR NAME</b>	<b>VENDOR NUMBER</b>
LRU	:TANK, 4.7 CUBIC FT. BRUNSWICK	MC282-0082-0010 BLD999020-1
LRU	:TANK, 4.7 CUBIC FT. ARDE	MC282-0082-0210 D4554

**EXTENDED DESCRIPTION OF PART UNDER ANALYSIS:**

HELIUM TANK, 4.7 CUBIC FEET, ENGINE SUPPLY, 4500 PSIA. LOCATED IN THE MID FUSELAGE.

**REFERENCE DESIGNATORS:** TK7  
TK9  
TK11

**QUANTITY OF LIKE ITEMS:** 3  
ONE PER ENGINE HE SUPPLY

**FUNCTION:**

STORES A PORTION OF THE HELIUM REQUIRED FOR MAIN ENGINE USAGE. ONE TANK, INTERCONNECTED WITH ANOTHER 4.7 (LOCATED IN THE AFT COMPARTMENT) AND A 17.3 CUBIC FOOT TANK (LOCATED IN THE MID FUSELAGE), IS DEDICATED TO EACH MAIN ENGINE. USES INCLUDE: PURGE OF LO2 HIGH PRESSURE OXIDIZER TURBOPUMP (HPOT) INTERMEDIATE SEAL; EMERGENCY SHUTDOWN; BLEED VALVE ACTUATION; FUEL SYSTEM PURGE (ANTI-ICE); AND POST SHUTDOWN HELIUM PURGE. RESIDUAL HELIUM WILL BE USED FOR MPS LINE REPRESSURIZATION AND ET UMBILICAL, OMS POD, AND AFT COMPARTMENT PURGES. TANK TK9 IS USED TO SUPPLEMENT THE PNEUMATIC HELLIUM SYSTEM BY CROSSOVER VALVE (LV10).

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**SUBSYSTEM NAME: MAIN PROPULSION**

**LRU: SSME HELIUM STORAGE TANK, 4.7 CUBIC FT.**

**CRITICALITY OF THIS**

**ITEM NAME: SSME HELIUM STORAGE TANK, 4.7 CUBIC FT.**

**FAILURE MODE: 1/1**

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**FAILURE MODE:**

RUPTURE/LEAKAGE

**MISSION PHASE:**

- PL PRE-LAUNCH
- LO LIFT-OFF
- OO ON-ORBIT
- DO DE-ORBIT
- LS LANDING/SAFING

**VEHICLE/PAYLOAD/KIT EFFECTIVITY:**

- 102 COLUMBIA
- 103 DISCOVERY
- 104 ATLANTIS
- 105 ENDEAVOUR

**CAUSE:**

MATERIAL DEFECT, FATIGUE

**CRITICALITY 1/1 DURING INTACT ABORT ONLY? NO**

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**REDUNDANCY SCREEN**

- A) N/A
- B) N/A
- C) N/A

**PASS/FAIL RATIONALE:**

A)

B)

C)

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**- FAILURE EFFECTS -**

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**(A) SUBSYSTEM:**

RESULTS IN LOSS OF HELIUM FROM ONE MAIN ENGINE'S HELIUM SUPPLY. POSSIBLE OVERPRESSURIZATION OF THE MID BODY, WING, AND AFT COMPARTMENT.

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RUPTURE OF HELIUM TANK MAY RESULT IN UNCONTAINED ENGINE SHUTDOWN DUE TO LOSS OF ENGINE HELIUM SUPPLY.

EXCESSIVE HELIUM LEAKAGE WILL BE DETECTABLE ON GROUND USING HAZARDOUS GAS DETECTION SYSTEM (HGDS). POSSIBLE MID BODY, WING, AND AFT COMPARTMENT OVERPRESSURIZATION AFTER HELIUM FILL. AFTER LIFTOFF, EXCESSIVE ENGINE HELIUM SUPPLY TANK AND/OR REGULATOR PRESSURE DECAY WILL BE INDICATED BY SM ALERT OR CAUTION AND WARNING.

DURING ENTRY, VENT DOORS ARE CLOSED TO PREVENT INGESTION OF RCS AND APU GASES. THIS FAILURE DURING THE TIME PERIOD THAT THE VENT DOORS ARE CLOSED MAY RESULT IN OVERPRESSURIZATION OF AFT COMPARTMENT. VENT DOORS ARE OPENED WHEN VEHICLE VELOCITY DROPS BELOW 2400 FT/SEC.

**(B) INTERFACING SUBSYSTEM(S):**  
SAME AS A.

**(C) MISSION:**  
POSSIBLE LAUNCH SCRUB DUE TO LCC VIOLATION. POSSIBLE ABORT DUE TO EARLY SHUTDOWN OF ONE ENGINE.

**(D) CREW, VEHICLE, AND ELEMENT(S):**  
POSSIBLE LOSS OF CREW/VEHICLE.

**(E) FUNCTIONAL CRITICALITY EFFECTS:**  
NONE.

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**-DISPOSITION RATIONALE-**

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**(A) DESIGN:**  
TYPE I TANK (BRUNSWICK)  
HE TANK LINER CONSISTS OF TWO FORGED HEMISPHERES FABRICATED FROM TITANIUM 6AL-4V ALLOY (0.05 INCH MINIMUM THICKNESS, 130 KSI ULTIMATE STRENGTH). THE TWO HEMISPHERES ARE WELDED TOGETHER. THE LINER IS WOUND WITH EPOXY-IMPREGNATED KEVLAR-49 FIBER (500 KSI TENSILE STRENGTH). FILAMENT WOUND CONSTRUCTION PRECLUDES FRAGMENTATION DAMAGE. THE DESIGN MEETS FRACTURE ANALYSIS REQUIREMENTS FOR 400 MISSIONS. FACTORS OF SAFETY ARE 1.33 PROOF AND 1.5 BURST.

TYPE III TANK (ARDE)  
HE TANK LINER CONSISTS OF TWO FORGED HEMISPHERES AND TWO END-SECTIONS FABRICATED FROM TYPE III CRYOFORMED 301 STAINLESS STEEL. THE TWO HEMISPHERES AND THE TWO SECTIONS ARE WELDED TOGETHER. THE LINER IS WOUND WITH GRAPHITE

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(MINIMUM 730,000 PSI TENSILE STRENGTH). FILAMENT WOUND CONSTRUCTION PRECLUDES FRAGMENTATION DAMAGE. THE DESIGN MEETS FRACTURE ANALYSIS REQUIREMENTS FOR 100 MISSIONS (FATIGUE TESTED FOR 400 MISSION). FACTORS OF SAFETY ARE 1.1 PROOF AND 1.5 BURST.

TO PRECLUDE RUPTURE THE PRESSURE VESSELS ARE DESIGNED TO ASSURE THAT UNDER NORMAL OPERATING CONDITIONS, ANY FAILURE RESULTING FROM METAL FATIGUE OR ANY OTHER DEFECTS WILL RESULT IN A LEAK BEFORE BURST FAILURE MODE. LEAK BEFORE BURST FAILURE MODE WAS DEMONSTRATED ON ONE BRUNSWICK TANK DURING TESTING.

**(B) TEST:**

ATP

- . LINER
  - . EXAMINATION OF PRODUCT
  - . CRYOSTRETCH VERIFICATION (TYPE III TANK ONLY): POST CRYOSTRETCH LINER VOLUME VERIFICATION AND LINER STRETCH DIMENSION VERIFICATION
  - . HEAT TREAT VERIFICATION COUPON TENSILE TEST
  - . WELD EVALUATION DIMENSIONALLY AND RADIOGRAPHICALLY INSPECTED
  - . PROOF PRESSURES: TYPE I TANK = 1057 PSIG; TYPE III TANK = 1185 PSIG.
  - . EXTERNAL LEAKAGE INTERNAL PRESSURES:
    - . TYPE I TANK = 953 PSIG (MAXIMUM LEAKAGE:  $1 \times 10^{-7}$  SCC/SEC OF HELIUM)
    - . TYPE III TANK = 1070 PSIG (MAXIMUM LEAKAGE.  $1 \times 10^{-6}$  SCC/SEC OF HELIUM)
  - . FLUORESCENT PENETRANT INSPECTION FOR SURFACE FLAWS
- . TANK
  - . EXAMINATION OF PRODUCT
  - . LEAKAGE TEST INTERNAL PRESSURE: 4500 PSIG MAXIMUM LEAKAGE (TYPE I TANK =  $1 \times 10^{-7}$  SCC/SECOND OF HELIUM, TYPE III TANK =  $1 \times 10^{-6}$  SCC/SECOND OF HELIUM)
  - . RADIOGRAPHIC INSPECTION INTERNAL PRESSURE:
    - . TYPE I TANK = 685 PSIG
    - . TYPE III TANK = 2610 PSIG.

CERTIFICATION

- . PRESSURE CYCLE TEST 1000 CYCLES PRESSURE RANGE: 0 TO 4500 PSIG  
PRESSURANT: WATER AT AMBIENT TEMPERATURE
- . EXTERNAL LEAKAGE INTERNAL PRESSURE:  
4500 PSIG MAXIMUM LEAKAGE (TYPE I TANK =  $1 \times 10^{-7}$  SCC/SECOND OF HELIUM, TYPE III TANK =  $1 \times 10^{-6}$  SCC/SECOND OF HELIUM)
- . CREEP TEST (TYPE III TANK ONLY): 90 DAYS INTERNAL PRESSURE: 4500 PSIG  
(HELIUM) AMBIENT TEMPERATURE
- . RANDOM VIBRATION 60 MINUTE IN EACH OF 2 AXES INTERNAL PRESSURE: 4500 PSIG
- . RADIOGRAPHIC INSPECTION
- . BURST/RUPTURE TEST PRESSURIZED UNTIL RUPTURE OCCURS

GROUND TURNAROUND TEST

ANY TURNAROUND CHECKOUT TESTING IS PERFORMED IN ACCORDANCE WITH OMRSD.

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**(C) INSPECTION:**

RECEIVING INSPECTION

MATERIALS AND PROCESS CERTIFICATIONS ARE VERIFIED BY INSPECTION. QUALITY TESTING PERFORMED ON FORGING IS VERIFIED BY INSPECTION. TYPE I TANK: MICRO-EXAMINATION AND CHEM-ETCH INSPECTION FOR ALPHA SEGREGATION IS VERIFIED BY INSPECTION

CONTAMINATION CONTROL

CLEANLINESS OF INTERNAL SURFACES TO LEVEL 100A IS VERIFIED BY INSPECTION. CORROSION PROTECTION PROVISIONS ARE VERIFIED BY INSPECTION.

ASSEMBLY/INSTALLATION

PART PROTECTION, MANUFACTURING PROCESSES, FINISHES, ASSEMBLY AND INSTALLATION PER SHOP TRAVELER ARE VERIFIED BY INSPECTION. PRESSURIZATION CYCLE HISTORY LOG AND SCHEDULES OF VESSELS ARE VERIFIED BY INSPECTION.

CRITICAL PROCESSES

WELDING, KEVLAR WRAPPING (TYPE I TANK) OR GRAPHITE WRAPPING (TYPE III TANK), EPOXY CURE PROCESS AND HEAT TREATMENT ARE VERIFIED BY INSPECTION. MECHANICAL PROPERTIES AND CHEMICAL ANALYSIS ARE VERIFIED BY INSPECTION AFTER FINAL HEAT TREATMENT.

NONDESTRUCTIVE EVALUATION

FLUORESCENT PENETRANT INSPECTION (SPECIAL LEVEL NDE) OF LINERS AND GIRTH WELDS, AND RADIOGRAPHIC INSPECTION OF GIRTH WELDS (BOTH BEFORE AND AFTER PROOF SIZING) ARE USED TO SCREEN POTENTIALLY DETRIMENTAL PARENT MATERIAL OR WELD DEFECTS. PROOF SIZING OF THE PRESSURE VESSEL ABOVE THE YIELD STRESS FOR THE LINER AIDS IN SCREENING FLAWS.

TESTING

ATP IS WITNESSED AND VERIFIED BY INSPECTION. PRESSURIZATION CYCLE HISTORY LOG AND SCHEDULE ARE VERIFIED BY INSPECTION.

HANDLING/PACKAGING

HANDLING, STORAGE, SHIPPING AND PACKAGING REQUIREMENTS ARE VERIFIED BY INSPECTION.

**(D) FAILURE HISTORY:**

CURRENT DATA ON TEST FAILURE, FLIGHT FAILURE, UNEXPLAINED ANOMALIES, AND OTHER FAILURES EXPERIENCED DURING GROUND PROCESSING ACTIVITY CAN BE FOUND IN THE PRACA DATABASE.

**(E) OPERATIONAL USE:**

NO CREW ACTION CAN BE TAKEN.

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**- APPROVALS -**

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S&R ENGINEERING	: W.P. MUSTY	:/S/ W. P. MUSTY
S&R ENGINEERING ITM	: P. A. STENGER-NGUYEN	:/S/ P. A. STENGER-NGUYEN
DESIGN ENGINEERING	: EARL HIRAKAWA	:/S/ EARL HIRAKAWA
MPS SUBSYSTEM MGR.	: TIM REITH	:/S/ TIM REITH
MOD	: BILL LANE	:/S/ BILL LANE
USA SAM	: MIKE SNYDER	:/S/ MIKE SNYDER
USA ORBITER ELEMENT	: SUZANNE LITTLE	:/S/ SUZANNE LITTLE
NASA SR&QA	: ERICH BASS	:/S/ ERICH BASS